

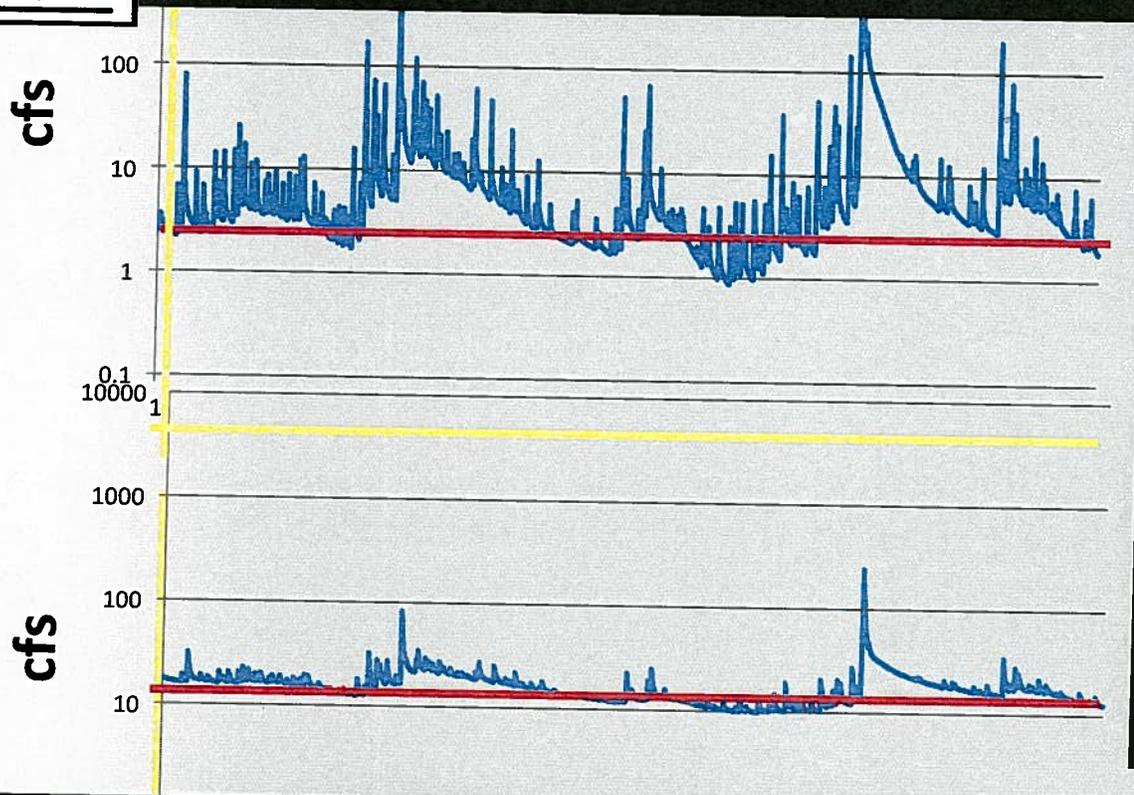
REVIEW OF THE MODEL RAISED A NUMBER OF CONCERNS I WILL SUMMARIZE AFTER EXPLAINING THE MOST IMPORTANT CONCERN

**WHICH IS IMPORTANT BECAUSE LOW FLOW MATTERS TO FISH HABITAT**

**THE MODEL IGNORES THE UNCONFINED AQUIFER BEHAVIOR OF SHALLOW ZONE**

SO FOR THE SAME CASE:

PROTESTANTS  
EXHIBIT  
10

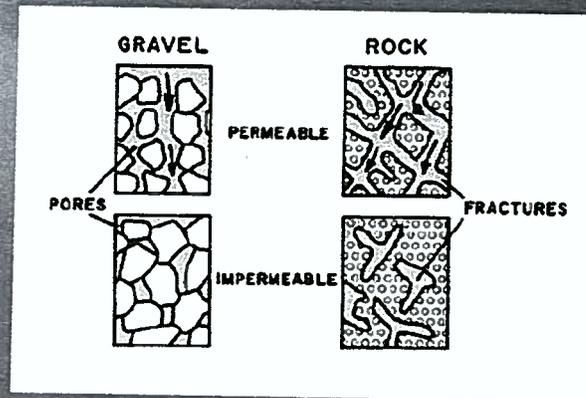


Without  
Unconfined Zone,  
BASEFLOW  
75% exceedance  
**2.5 cfs**

With  
Unconfined Zone,  
BASEFLOW  
75% exceedance  
**13.2 cfs**

**AVERAGE ANNUAL BASEFLOW IS THE SAME FOR BOTH CASES**  
If average base flow is of interest THEN only recharge matters  
**AND WE DO NOT NEED A NUMERICAL MODEL**

# Aquifer hydraulic properties: Storage coefficient



The volume of water given up per unit area of an aquifer per unit drop of the water-table or potentiometric surface.

# Aquifer Hydraulic Properties: Storage Coefficient

Alluvial aquifer	0.2
Arbuckle- Simpson aquifer	0.008

Not just a matter of  
Alluvial vs Arbuckle-Simpson

ALSO

UNCONFINED vs CONFINED

1 SQUARE  
FOOT



ENTIRE  
THICKNESS

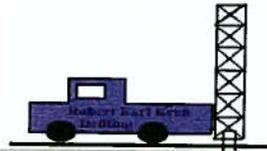


Alluvial aquifer  
1.5 gallons



Arbuckle-Simpson aquifer  
1 cup

# ALL HYDROLOGISTS TESTIFYING YESTERDAY AGREED THE SHALLOW ZONE IS UNCONFINED



NOT TO SCALE

SHALLOW ZONE  
Unconfined (water table)      Lower hydraulic conductivity K  
Higher Specific Storage Ss

DEEPER ZONE  
Confined      Higher hydraulic conductivity K  
Lower Specific Storage Ss

BEDROCK

Fairchild and others (1990) reported that “information from drillers and land owners suggests that the upper few hundred feet of the Arbuckle Group has a much lower permeability than the lower part.”

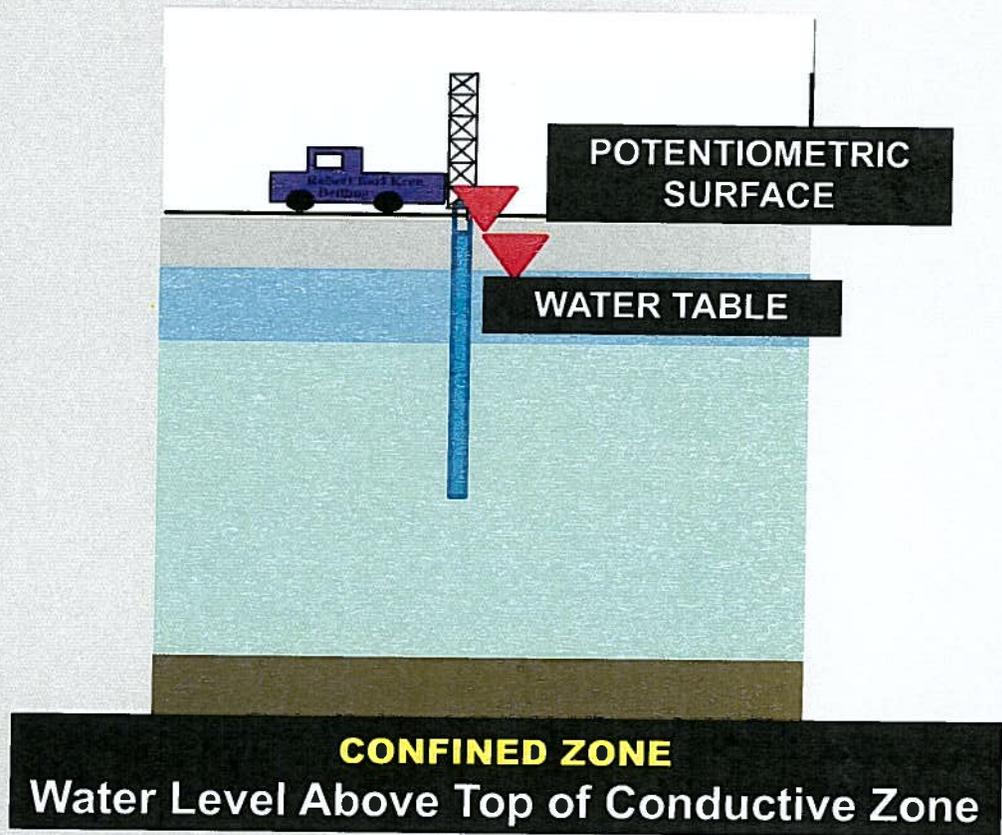
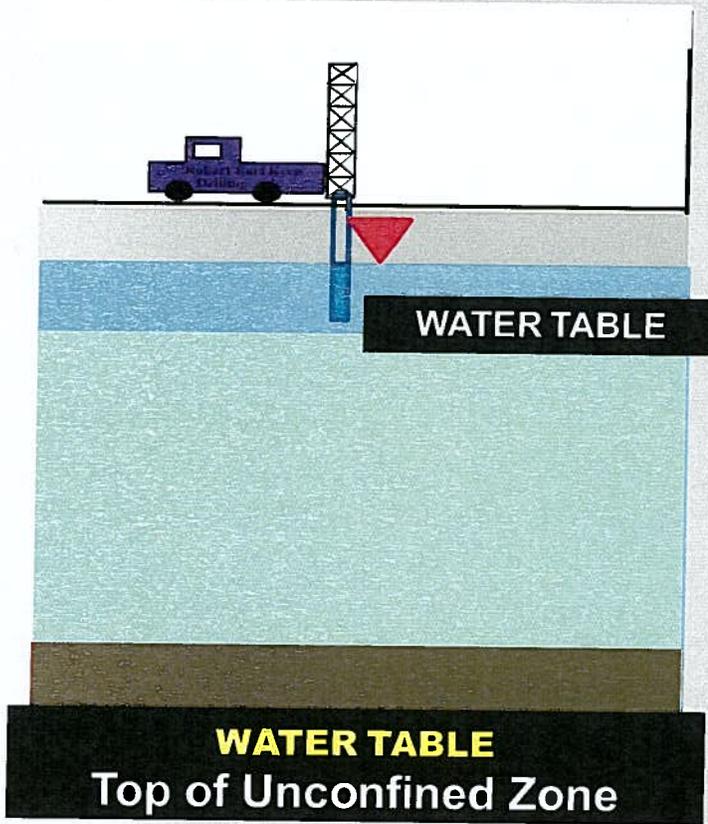
**K is permeability, also called hydraulic conductivity**

**K is ability to push water through**

**Ss = Specific Storage is ability to store water per unit of thickness**

**S = Storage Coefficient is ability to store water in entire thickness**

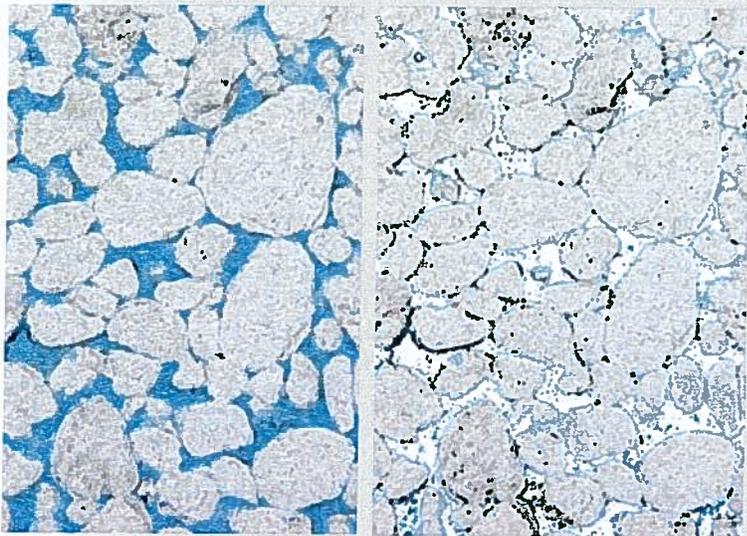
**$S = Ss \times \text{Thickness}$**



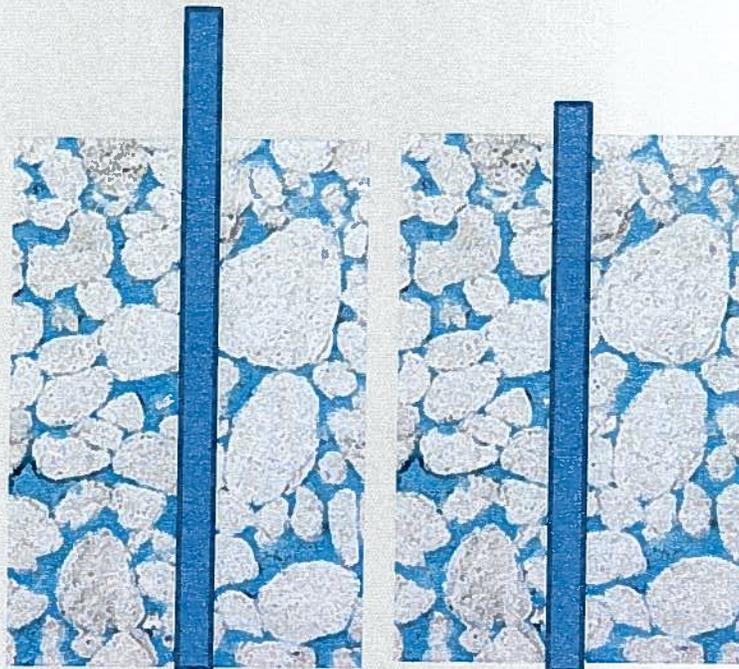
**NOT TO SCALE**

# ALL HYDROLOGISTS TESTIFYING YESTERDAY AGREED PORES DRAIN WHEN WATER LEVEL DECLINES IN UNCONFINED ZONE

UNCONFINED AQUIFER  
PORES DRAIN WHEN WATER  
LEVEL LOWERS



CONFINED AQUIFER  
PORES DO NOT DRAIN WHEN  
WATER LEVEL LOWERS

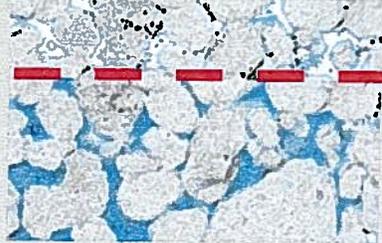


**UNCONFINED BEFORE  
WATER LEVEL DECLINE**

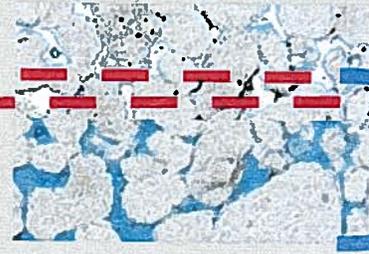
**AFTER 1 FOOT DECLINE**

**IN THE  
UNCONFINED  
ZONE**

**WHEN WATER  
LEVEL  
DECLINES  
WATER DRAINS  
FROM PORES**



**100  
FEET**



**1 FOOT**

**STORAGE  
Essentially  
ALL FROM  
TOP  
1 FOOT**



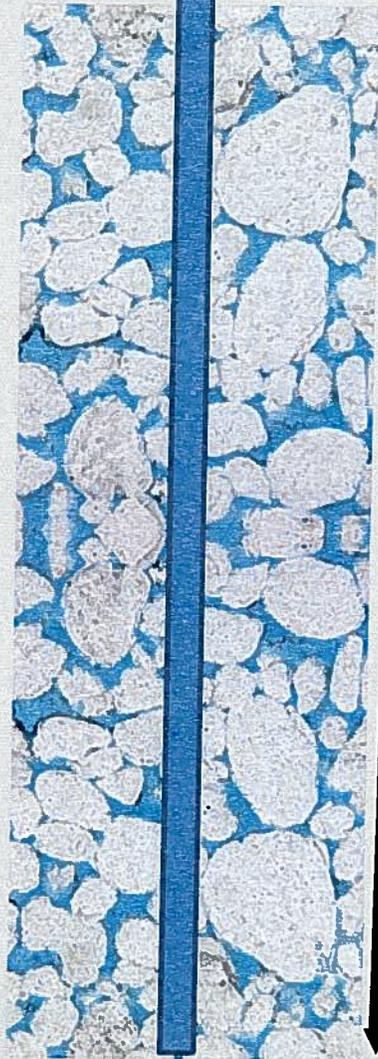
1.5 gallons

**CONFINED BEFORE  
WATER LEVEL DECLINE**

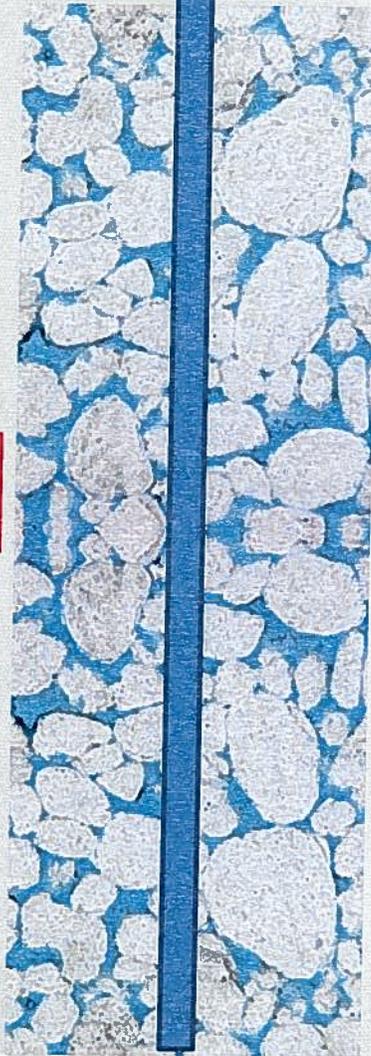
**AFTER 1 FOOT DECLINE**

**1 FOOT**

**CONFINED ZONE**  
WHEN WATER LEVEL DECLINES  
AQUIFER COMPRESSES AND  
WATER EXPANDS TO PROVIDE  
WATER  
**PORES DO NOT DRAIN**



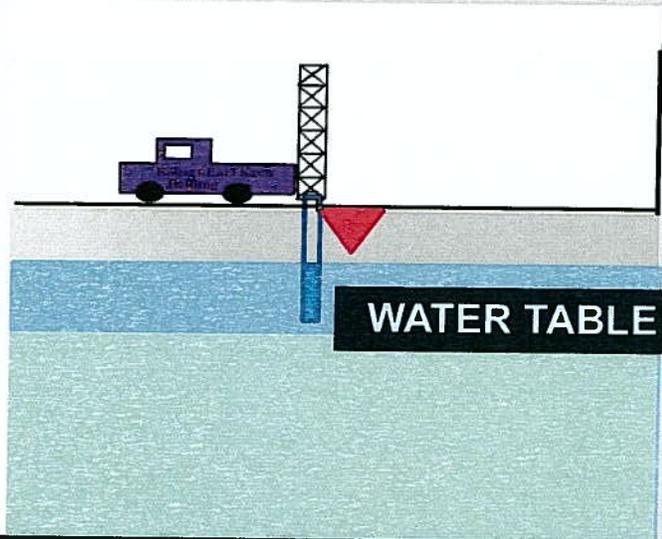
**3500  
FEET**



**STORAGE  
released  
from entire  
aquifer  
thickness**

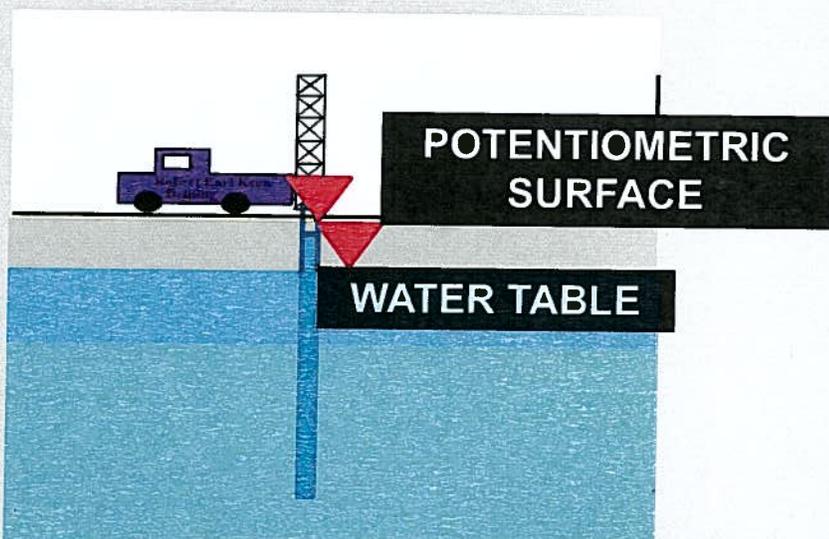
  
**1 cup**

**NOT TO SCALE**



FEW WELLS ARE COMPLETED IN THE UNCONFINED ZONE IN THE STUDY AREA BECAUSE LOW K MAKES THEM LESS DESIRABLE FOR WATER SUPPLY

ONE WELL IN THIS ZONE  
OWRB 85182, 53 FT DEEP  
STORAGE COEFFICIENT 0.075



NEARLY ALL WELLS OF STUDY AREA ARE IN THE CONFINED ZONE

MANY MEASUREMENTS OF THIS STORAGE COEFFICIENT RANGE FROM 0.002 to 0.02

0.075 is NOT a very small value as was stated yesterday  
It does NOT indicate a confined condition as was stated yesterday  
It is indicative of unconfined conditions

USGS used CONFINED MODFLOW layers to simulate the UNCONFINED portion of the Arbuckle-Simpson aquifer

STATED THIS WAS BECAUSE:

Storage coefficients similar

Drawdown would be small

The model solution will be more stable

Using confined MODFLOW layers is acceptable as long as storage in the top layer represents drainage of water from the pores, but this was not done in the USGS model, so the streams were too sensitive to pumping.

As three hydrologists noted yesterday Storage Coefficient is typically much higher in unconfined zone.

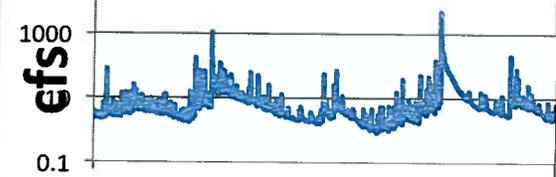
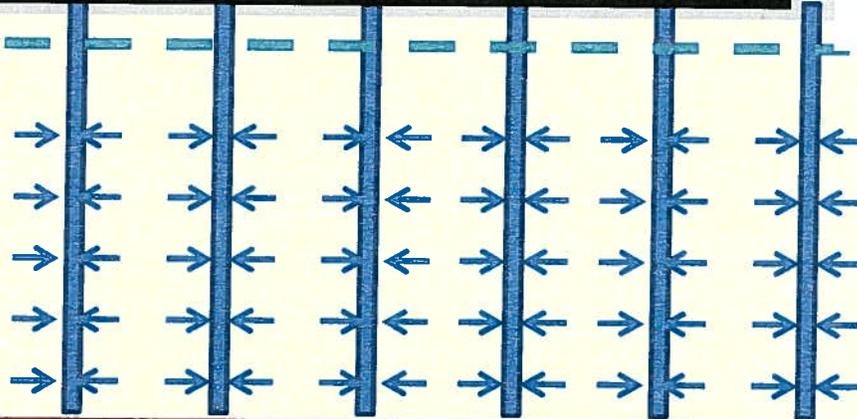
Even if the S values are both 0.008, the Ss value was entered incorrectly in MODFLOW, making S of the top layer only 2% of what it should be.

If S of top layer is 0.008, Ss should be  $0.008/20\text{m} = 0.0004\text{m}^{-1}$ , not  $0.000008\text{m}^{-1}$

This required procedure for input of S of the top layer is demonstrated by the SYTP parameter in the MODFLOW HUF2 package.

**When the water table is not considered in the model stream base flow variation is larger because the buffer provided by unconfined storage is ignored**

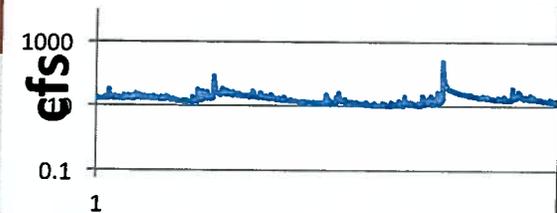
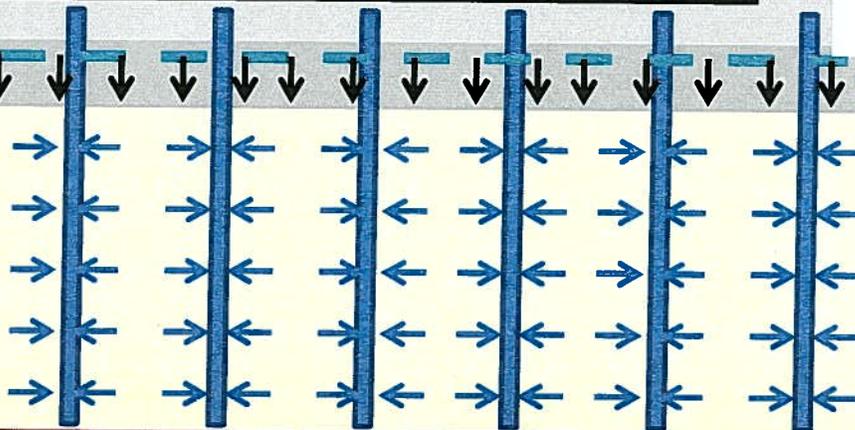
Unconfined layer ignored



**Drainage of pore water from the unconfined zone BUFFERS the stream base flow from seasonal pumping**

Unconfined Included

Confined zone



I ran simulations to determine the influence  
of representing the top layer as unconfined

**SIMULATION INVOLVED:**

Running the transient calibration model with the 0.392 (A-F/A)/Yr, eps  
Repeating until the cumulative budget did not change

**RUN #1**

USGS Model Storage Properties

Storage coefficient of 0.008 and a thickness of 1000m

ALL LAYERS  $S_s = S/thk = 0.000008$

**RUN #2**

USGS Field Measured Storage Properties

Storage coefficient of 0.075 and a thickness of 20m

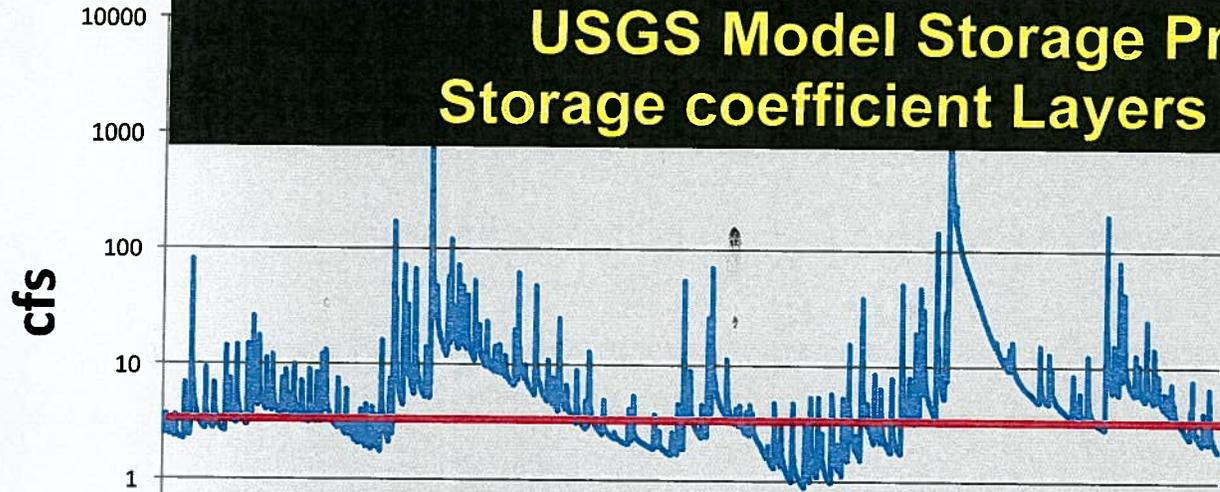
TOP LAYER  $S_s = S/thk = 0.00375$

Storage coefficient of 0.011 and a thickness of 1040m

LAYERS BELOW TOP  $S_s = S/thk = 0.00001056$

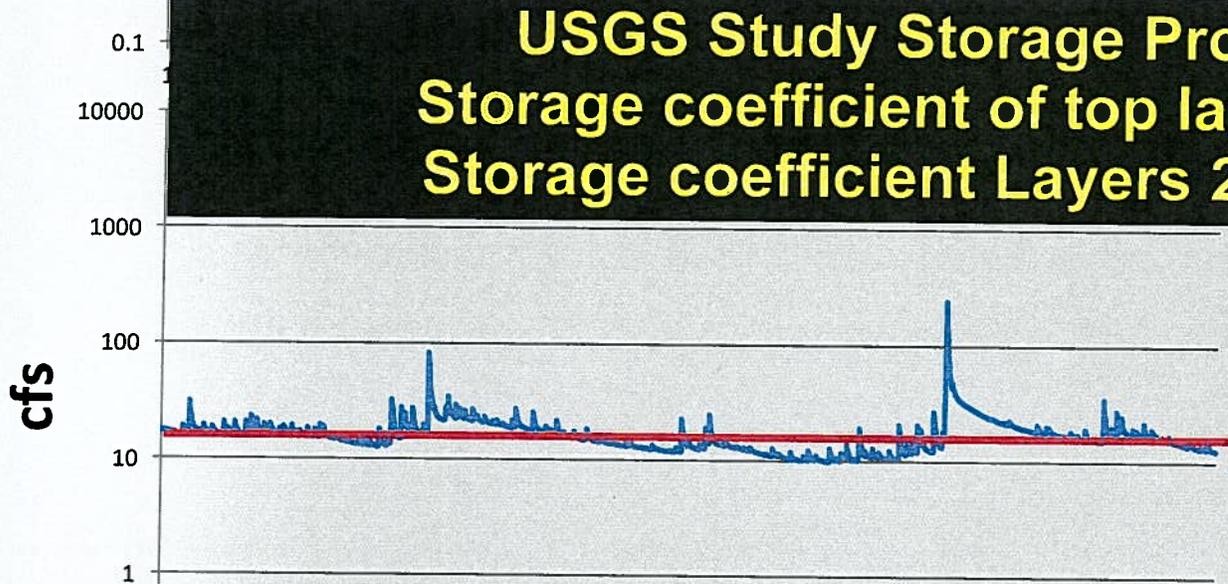
# Blue River @ Connerville Oct 2003 to Oct 2008

## USGS Model Storage Properties Storage coefficient Layers 1-6 = 0.008



EPS = 3.92 AFY  
Without unconfined  
zone, BASEFLOW  
75% exceedance **2.5**  
cfs

## USGS Study Storage Properties Storage coefficient of top layer = 0.075 Storage coefficient Layers 2-6 = 0.011



EPS = 3.92 AFY  
With unconfined  
zone, BASEFLOW  
75% exceedance **13.2**  
cfs

## **RESULTS OF THE SIMULATION DO NOT PROVIDE INFORMATION ON THE EXPECTED BASE FLOW**

**The point is not that we have the right values, rather that including the unconfined zone while using reasonable S values, properly input, makes a substantial difference in low flow of streams**

**Storage coefficient of unconfined zone  
needs to be better measured in the field  
and properly input to MODFLOW**

**Storage Coefficients need to be included  
in the calibration process.**

## **Stream conductance**

**Units given in report were incorrect (m/d, should be m<sup>2</sup>/d)**

**A constant value of 1000 was used and not explained  $C = KLW/b$**

## **Steady State Calibration**

**Steady State simulation used 4 time steps, only one is needed**

**Unsubstantiated "steady-state" data for steady-state calibration**

**Multi-level nature of observation data was not included in the model**

**Parameter estimation process was not presented nor files provided**

**Residuals exhibited spatial bias**

**The guidance for effective model calibration of Hill and Tiedeman 2007 was not followed**

**Steady state and transient calibrations were not combined**

## **Transient Calibration**

**Initial conditions for transient simulation were not generated properly**

**Only two transient calibration targets were used, transient head data were not used**

**Transient calibration did not optimize the value of storage coefficient**

**Prediction sensitivities were not provided so we do not know which parameters influenced the predictions**

**Uncertainty in predictions was not presented**

## **CONCLUSION**

**Given the importance of determining a safe and fair equal proportionate share, the model evaluation should be rigorous.**

**The model is not ready for use in making policy decisions until**

**storage coefficients have been properly measured and  
incorporated in the model**

**shortcomings outlined in previous slide are addressed**