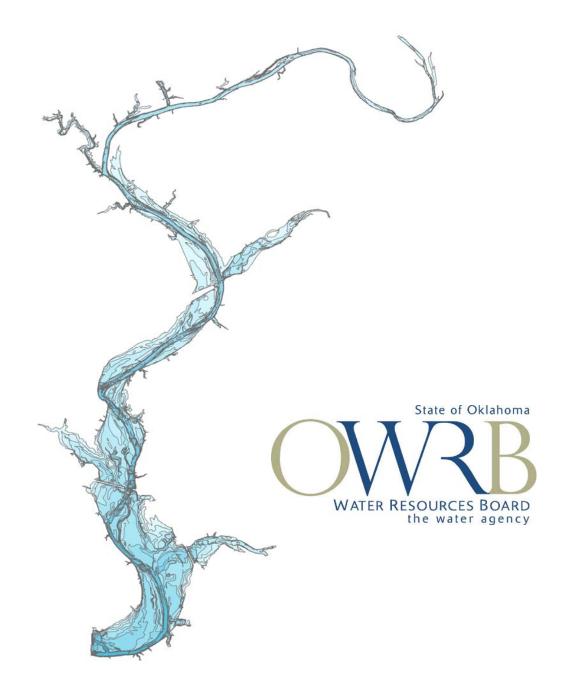
HYDROGRAPHIC SURVEY OF LAKE HUDSON



Final Report

October 23, 2008

Prepared by: Oklahoma Water Resources Board

TABLE OF CONTENTS

TABLE OF CONTENTS	2
TABLE OF FIGURES	3
TABLE OF TABLES	3
INTRODUCTION	4
LAKE BACKGROUND	4
History	4
Lake Information	4
HYDROGRAPHIC SURVEYING PROCEDURES	6
Pre-survey Planning	
Boundary File	6
Set-up	6
Field Survey	6
Method	6
Technology	6
Survey	
Quality Control/Quality Assurance	
Data Processing	10
GIS Application	10
RESULTS	11
SUMMARY	11
REFERENCES	
APPENDIX A: Sound Velocity Profile	
APPENDIX B: Area-Capacity Data	20
APPENDIX C: Lake Hudson Bathymetric Maps	26

TABLE OF FIGURES

Figure 1:	Location map for Lake Hudson.	5
_	Histogram of relative depth distribution at cross check lines - in standard deviation	
Figure A.	1: Sound Velocity Profiles for November 6, 7, 8, and 13, 2006	16
Figure A.	2: Sound Velocity Profiles for November 14, 27, 28, and 29, 2006	17
Figure A.	3: Sound Velocity Profiles for December 5, 6, 12, and 13, 2006	18
Figure A.	4: Sound Velocity Profiles for December 14, 2006 and March 28 and 29, 2007	19
Figure B.	1. Capacity-Area Curve	25
Figure C.	1: Lake Hudson Bathymetric Map with 5-foot Contour Intervals	27
-	2: Lake Hudson Shaded Relief Bathymetric Map.	
Figure C.	3: Lake Hudson Collected Data Points.	29

TABLE OF TABLES

Table 1: Area and Volume Comparisons of Lake Hudson at Conservation Pool Elevation (619.0 ft).	
Table A. 1: Sound Velocity Profile Data (ft/sec) for November 6 – 29, 2006	
Table A. 2: Sound Velocity Profile Data (ft/sec) for December 5, 2006 - March 29, 2007	
Table B. 1: Lake Hudson Capacity/Area by 0.1-ft Increments	21
Table B. 2: Lake Hudson Capacity/Area by 0.1-ft Increments (cont)	21
Table B. 3: Lake Hudson Capacity/Area by 0.1-ft Increments (cont)	22
Table B. 4: Lake Hudson Capacity/Area by 0.1-ft Increments (cont).	23

LAKE HUDSON (MARKHAM FERRY RESERVOIR) HYDROGRAPHIC SURVEY REPORT

INTRODUCTION

The Oklahoma Water Resources Board (OWRB) conducted a hydrographic survey of Lake Hudson (Markham Ferry Reservoir) from November to December of 2006 and March of 2007. The purpose of the study was to collect hydrographic data of Lake Hudson and convert this information into an area-elevation-volume table up to the conservation pool elevation. The information produced will serve as a base to establish the location and rate of sedimentation in the conservation pool for future surveys.

LAKE BACKGROUND

History

On August 18, 1941, the Flood Control Act authorized the construction of what was initially called the Markham Ferry Reservoir. In July of 1946, it was incorporated into the Arkansas River multi-purpose plan by the River and Harbor Act. The Lake's authorization was further modified in July 1954 by Public Law 476. This authorized the Grand River Dam Authority (GRDA) to construct Lake Hudson. Construction of Lake Hudson began in January of 1962 and was completed in 1964 (USACE, 1992). The lake is used for flood control and hydroelectric power and was authorized by the Flood Control Act approved August 18, 1941. The lake is a multi-purpose project for flood control, hydropower, and navigation.

Lake Information

Lake Hudson is located in Mayes County in the Arkansas River Basin on Grand (Neosho) River. The Robert S. Kerr Dam located on Lake Hudson is approximately 2 miles northwest of Locust Grove and 8 miles southeast of Pryor. A general location map of Lake Hudson is shown on the following page as **Figure 1**. Based on the original sediment surveys, Lake Hudson covers an area of 10,900 acres and has a capacity of 200,400 acre-feet at the top of the conservation pool elevation of 619 ft NGVD. The reservoir has a length of 29.6 miles and an estimated total of 200 miles of shoreline at the top of the conservation pool (USACE, 1992).

GRDA owns and is the regulating agency of Lake Hudson. The Tulsa District of the US Army Corps of Engineers (USACE), by authority of the Flood Control Act of 1944 (Public Law 78-534, 58 Stat. 890, 33 U.S.C. 709), is responsible for prescribing regulation for the use of the flood control storage in the lake between elevations 619 and 636 ft NGVD (USACE, 1992).

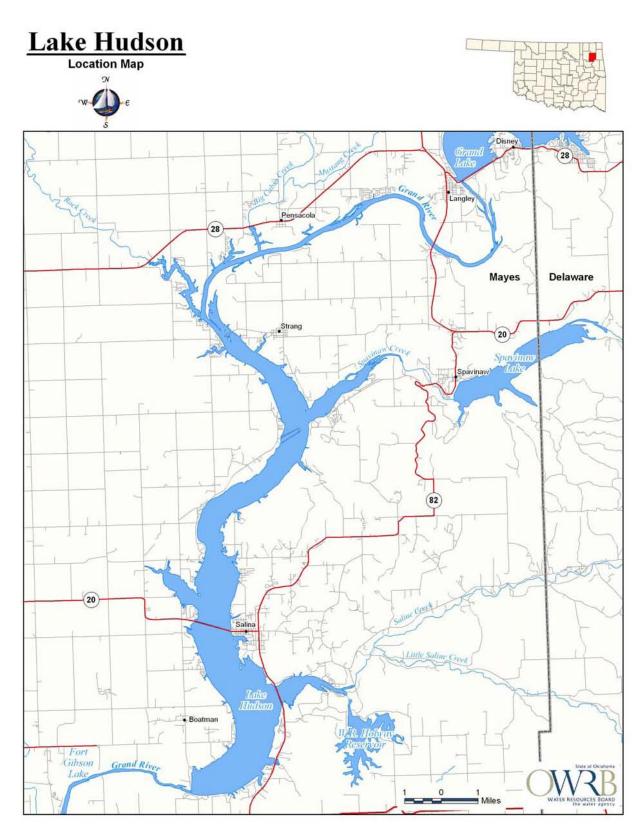


Figure 1: Location map for Lake Hudson.

HYDROGRAPHIC SURVEYING PROCEDURES

The process of surveying a reservoir uses a combination of Geographic Positioning System (GPS) and acoustic depth sounding technologies that are incorporated into a hydrographic survey vessel. As the survey vessel travels across the lake's surface, the echosounder gathers multiple depth readings every second. The depth readings are stored on the survey vessel's on-board computer along with the positional data generated from the vessel's GPS receiver. The collected data files are downloaded daily from the computer and brought to the office for editing after the survey is completed. During editing, data "noise" is removed or corrected, and average depths are converted to elevation readings based on the daily-recorded lake level elevation on the day the survey was performed. Accurate estimates of area-capacity can then be determined for the lake by building a 3-D model of the reservoir from the corrected data. The process of completing a hydrographic survey includes four steps: pre-survey planning, field survey, data processing, and GIS application.

Pre-survey Planning

Boundary File

The digitized boundary of Lake Hudson was produced from the 1995 black and white US Geological Survey (USGS) digital ortho quarter quads (DOQQs) of Mayes County, Oklahoma at a scale of 1:1,500. The lake elevation at the time of the 1995 DOQQ was 619.17 ft NGVD. The reservoir boundary was digitized in NAD 1983 State Plane Coordinates (Oklahoma North-3501). The 2003 United States Department of Agriculture-Farm Service Agency-Aerial Photography Field Office (USDA-FSA-APFO) color DOQQ of Mayes County was also used for reference. The lake elevation at the time the 2003 DOQQ was taken was 619.9 ft NGVD.

Set-up

HYPACK software from Hypack, Inc. was used to assign geodetic parameters, import background files, and create virtual track lines (transects). The geodetic parameters assigned were State Plane NAD 83 Zone OK-3501 Oklahoma North with distance units and depth as US Survey Feet. The survey transects were spaced according to the accuracy required for the project. The survey transects within the digitized reservoir boundary were at 500 ft increments and ran perpendicular to the original stream channels and tributaries. Approximately 285 virtual transects were created for the Lake Hudson project not including channel track lines, which were created after the initial surveying of the lake transects.

Field Survey

Method

The procedures followed by the OWRB during the hydrographic survey adhere to U.S. Army Corps of Engineers (USACE) standards (USACE, 2002). The quality control and quality assurance procedures for equipment calibration and operation, field survey, data processing, and accuracy standards are presented in the following sections.

Technology

The Hydro-survey vessel was an 18-ft aluminum Silverstreak hull with cabin, powered by a single 115-Horsepower Mercury outboard motor. Equipment used to conduct the survey included: a ruggedized notebook computer; Syqwest Bathy 1500 Echo Sounder, with a depth resolution of 0.1 ft; Trimble Navigation, Inc. Pro XR GPS receiver with differential global

positioning system (DGPS) correction; and an Odom Hydrographics, Inc, DIGIBAR-Pro Profiling Sound Velocimeter. A 12V battery and inverter provided the power supply to the equipment. The software used was HYPACK.

Survey

A two-man survey crew was used during the project. Data collection for Lake Hudson occurred on 11/06-08/2006, 11/13-14/2006, 11/27-29/2006, 12/05-06/2006, 12/13-14/2006, and 2/28-29/2007. The average water level elevation in November and December 2006 was approximately 618.4 ft NGVD. The average elevation in March 2007 was approximately 619 ft NGVD. Data collection began at the dam and moved north up the reservoir. The survey crew followed the parallel transects created during the pre-survey planning while collecting depth soundings and positional data. Data was also collected along a path parallel to the shoreline at a distance that was determined by the depth of the water and the draft of the boat. This was usually in a water depth of two to three feet. Areas with depths less than what could accommodate the boat were avoided.

Quality Control/Quality Assurance

While on board the Hydro-survey vessel, the Syqwest Bathy 1500 Echo Sounder was calibrated using A DIGIBAR-Pro Profiling Sound Velocimeter, by Odom Hydrographics. The sound velocimeter measures the speed of sound at incremental depths throughout the water column. The factors that influence the speed of sound—depth, temperature, and salinity—are all taken into account. Deploying the unit involved lowering the probe, which measures the speed of sound, into the water to the calibration depth mark to allow for acclimation and calibration of the depth sensor. The unit was then gradually lowered at a controlled speed to a depth just above the lake bottom, and then was raised to the surface. The unit collected sound velocity measurements in feet/seconds (ft/sec) at 1 ft increments on both the deployment and retrieval phases. The data was then reviewed for any erroneous readings, which were then edited out of the sample. The sound velocity corrections were then applied to the to the raw depth readings. The average speed of sound in the water column ranged from 4,711.7 ft/sec to 4,808.5 ft/sec during the Lake Hudson survey. The sound velocity profiles for each date of surveying are shown in **APPENDIX A: Sound Velocity Profile**.

A quality assurance cross-line check was undertaken on intersecting transect lines and channel track lines to assess the estimated accuracy of the survey measurements. The overall accuracy of an observed bottom elevation or depth reading is dependent on many random and systematic errors that are present in the measurement processes used to determine that depth readings. Depth measurements contain both random errors and systematic bias. Biases are often referred to as systematic errors and are often due to observational errors. Examples of bias include a bar check calibration error, tidal errors, or incorrect squat corrections. Bias, however, does not affect the repeatability, or precision, of results. The precision of depth readings is affected by random errors. These are errors present in the measurement system that cannot be easily reduced by further calibration. Examples of random error include uneven bottom topography, bottom vegetation, positioning error, extreme listing of survey vessel, and speed of sound variation in the water column. An assessment of the accuracy of an individual depth or bottom elevation must fully consider all the error components contained in the observations that were used to determine that measurement. Therefore, the ultimate accuracy must be estimated (thus the use of the term "estimated accuracy") using statistical estimating measures (USACE, 2002).

The depth accuracy estimate is determined from comparing depth readings between readings taken at an intersection of two lines and computing the difference. The mean difference of all intersection points used to calculate the mean difference (MD). The mean difference represents the bias present in the survey. The standard deviation (SD), representing the random error in the survey, is also calculated. The mean difference and the standard deviation are then used to calculate the Root Mean Square (RMS) error. The RMS error estimate is used to compare relative accuracies of estimates that differ substantially in bias and precision (USACE, 2002). According the USACE standards, the RMS should not exceed a tolerance of \pm 2.0 ft for this type of survey. This is done to verify compliance with the resultant depth accuracy of \pm 2.0 ft at the 95% confidence level. This simply means that on average, 19 of every 20 observed depths will fall within the specified accuracy tolerance.

HYPACK Cross Statistics program was used to assess vertical accuracy and confidence measures of acoustically recorded depths. The program computes the sounding difference between intersecting lines of single beam data. The program provides a report that shows the standard deviation and mean difference. A total of 114 cross-sections points were used to compute error estimates. A mean difference of 0.0 ft and a standard deviation of 1.09 ft were computed from a number of 114 data points. Using the following formulas, a 95% depth accuracy of \pm 2.1 ft was calculated.

$$RMS = \sqrt{SD^2 + MD^2}$$

RMS (95%) depth accuracy = $1.96 \times RMS$

where:

MD = mean differenceSD = standard deviationRMS = root mean square error

An RMS of \pm 2.1 ft with a 95% level is slightly higher than the USACE's minimum performance standard of \pm 2.0 ft for this type of survey. A mean difference, or bias, of 0.0 ft is well below the USACE's standard maximum allowable bias of \pm 0.5 ft for this type of survey. It must be remembered that minimizing constant bias errors is far more important than reducing deviations (USACE, 2002). The data plotted in **Figure 2** illustrates that the measurements have somewhat low precision but high accuracy (USACE, 2002).

Quality Assurance Cross-line Check

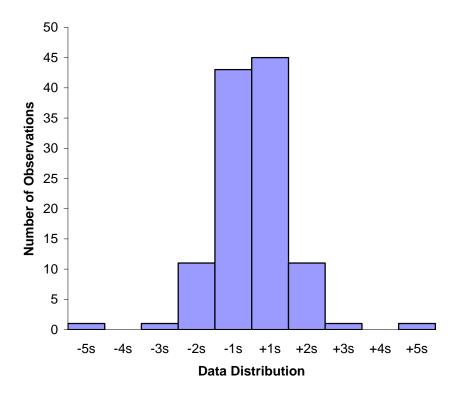


Figure 2: Histogram of relative depth distribution at cross check lines - in standard deviation.

The GPS system is an advanced high performance geographic data-acquisition tool that uses DGPS to provide sub-meter positional accuracy on a second-by-second basis. Potential errors are reduced with differential GPS because additional data from a reference GPS receiver at a known position are used to correct positions obtained during the survey. Before the survey, Trimble's Pathfinder Controller software was used to configure the GPS receiver. To maximize the accuracy of the horizontal positioning, the horizontal mask setting was set to 15 degrees and the Position Dilution of Precision (PDOP) limit was set to 6. The position interval was set to 1 second and the Signal to Noise Ratio (SNR) mask was set to 4. The United States Coast Guard reference station used in the Lake Hudson survey is located near Sallisaw, Oklahoma. The reference beacon system transmitted corrected signals in real time, so no post-processing corrections of position data were needed. The collected DGPS positions were converted to state-plane coordinate system using the HYPACK program.

A latency test was performed to determine the fixed delay time between the GPS and single beam echo sounder. The timing delay was determined by running reciprocal survey lines over a channel bank. The raw data files were downloaded into HYPACK, LATENCY TEST program. The program varies the time delay to determine the "best fit" setting. A position latency of 0.1 seconds was produced and adjustments were applied to the raw data in the EDIT program.

Data Processing

The collected data was downloaded from the field computer onto the OWRB computer network and data burned to a CD as a permanent record. After downloading the data, each raw data file was reviewed for accuracy and completeness using the EDIT program within HYPACK. The EDIT program allowed the user to assign transducer offsets, latency corrections, tide corrections, display the raw data profile, and review/edit all raw X, Y, and Z information. Collected data points that have inaccurate or absent depth or positional information were interpolated to be congruent with adjacent accurate points or deleted completely.

Offset correction values of 3.2 ft. starboard, 6.6 ft. forward, and -1.1 ft. vertical were applied to all raw data along with a latency correction factor of 0.1 seconds. The speed of sound readings from the sound profiling velocimeter are documented in **APPENDIX A: Sound Velocity Profile**.

Using HYPACK, TIDES program, a tide correction file was produced to account for the variance in lake elevation at the time in which data was collected. Within the EDIT program, the corrected depths were subtracted from the elevation reading to convert the depth in feet to an elevation.

After editing the data for errors and correcting the spatial attributes (offsets and tide corrections), a data reduction scheme was needed. To accomplish this the data was resampled spatially at a 10 ft interval using the Sounding Selection program in HYPACK. The resultant data was saved and exported out as a xyz.txt file. The HYPACK data file for Lake Hudson is located at the end of the document on the CD entitled *Hudson HYPACK/GIS Metadata*.

GIS Application

Geographic Information System (GIS) software was used to process the edited XYZ data collected from the survey. The GIS software used was ArcGIS Desktop and ArcMap, version 9.1, from Environmental System Research Institute (ESRI). All of the GIS datasets created are in Oklahoma State Plane North Coordinate System referenced to the North American Datum 1983. Horizontal and vertical units are in feet. The edited data points in XYZ text file format were converted into ArcMap point coverage format. The point coverage contains the X and Y horizontal coordinates and the elevation and depth values associated with each collected point.

Volumetric and area calculations were derived using a TIN surface model. The TIN model was created in ArcMap, using the collected survey data points and the lake boundary inputs. The TIN consists of connected data points that form a network of triangles representing the bottom surface of the lake. Approximately 131,373 data points were used to create the TIN model. The lake volume was calculated by slicing the TIN horizontally into planes 0.1 ft thick. The volume and area of each slice are shown in **APPENDIX B: Area-Capacity Data**.

Contours, depth ranges, and the shaded relief map were derived from a digital elevation model grid. This grid was created using the ArcMap Topo to Raster Tool and had a spatial resolution of five feet. A low pass 3x3 filter was run to lightly smooth the grid to improve contour generation. The contours were created at a 5-ft interval using the ArcMap Contour Tool. The contour lines were edited to allow for polygon topology and to improve accuracy

and general smoothness of the lines. The contours were then converted to a polygon coverage and attributed to show 5-ft depth ranges across the lake. The bathymetric map of the lake is shown with 5-ft contour intervals in Appendix C.

All geographic datasets derived from the survey contain Federal Geographic Data Committee (FGDC) compliant metadata documentation. The metadata describes the procedures and commands used to create the datasets. The GIS metadata file for Lake Hudson is located at the end of the document on the CD entitled *Hudson HYPACK/GIS Metadata*.

RESULTS

Results from the 2006-2007 OWRB survey indicate that Lake Hudson encompasses 11,029 acres and contains a cumulative capacity of 200,185 ac-ft at the conservation pool elevation (619 ft NGVD). The average depth for Lake Hudson was 18.2 ft with a maximum depth of 65 ft.

SUMMARY

Table 1 summarizes all surveys conducted of Lake Hudson at the conservation pool elevation. Based on the original sediment survey, Lake Hudson had an area of 10,900 acres and cumulative volume of 200,400 acre-feet of water at conservation pool elevation (USACE, 1992). The surface area of the lake has increased 1.5% or approximately 164 acres. Hudson Lake has had a less than a 0.1% decrease in capacity or a loss of approximately 178 acre-feet. However, caution should be used when directly comparing between the original survey and the 2006-2007 survey conducted by the OWRB. Different methods were used to collect the data and extrapolate capacity and area figures. It is the recommendation of the OWRB that another survey using the same method used in the 2006-2007 survey be conducted in 15 years.

Table 1: Area and Volume Comparisons of Lake Hudson at Conservation Pool Elevation (619.0 ft).

Feature	Survey Year					
	Original Survey	2006-2007				
Area (acres)	10,865	11,029				
Cumulative Volume (acre-feet)	200,363	200,185				
Mean depth (ft)	18.44	18.15				

REFERENCES

U.S. Army Corps of Engineers (USACE). 1992. Water Control Manual – Markham Ferry Reservoir.

U.S. Army Corps of Engineers (USACE). 2002. Engineering and Design - Hydrographic Surveying, Publication EM 1110-2-1003, $3^{\rm rd}$ version.

APPENDIX A: Sound Velocity Profile

Table A. 1: Sound Velocity Profile Data (ft/sec) for November 6-29, 2006.

Depth	11/06/2006	11/07/2006	11/08/2006	11/13/2006	11/14/2006	11/27/2006	11/28/2006	11/29/2006
1	4802.8		4800.1	4795.5	4790.6	4784.1	4789.7	4794.7
2	4802.5	4802.7	4800.1	4795.5	4790.8	4784.0	4789.6	4794.7
3	4802.2	4801.6	4800.1	4795.5	4790.8	4783.7	4789.5	4794.7
4	4802.1	4801.4	4800.1	4795.5	4790.8	4783.3	4789.4	4794.6
5	4802.0	4801.1	4800.1	4795.1	4790.9	4783.0	4789.3	4794.6
6	4801.7	4801.0	4800.1	4794.8	4790.9	4782.5	4789.2	4794.6
7	4801.4	4800.9	4800.1	4794.8	4791.0	4782.1	4789.2	4794.6
8	4801.2	4800.8	4800.1	4794.8	4791.1	4782.0	4789.0	4794.6
9	4801.1	4800.8	4800.2	4794.5	4791.2	4782.0	4789.0	4794.6
10	4801.1	4800.7	4800.2	4794.5	4791.3	4781.8	4789.0	4794.6
11	4801.1	4800.7	4800.2	4794.5	4791.2	4781.7	4788.9	4794.6
12	4801.0	4800.7	4800.3	4794.5	4791.2	4781.7	4788.9	4794.6
13	4801.1	4800.7	4800.3	4794.5	4791.3	4781.7	4788.8	4794.5
14	4801.1	4800.7	4800.3	4794.5	4791.2	4781.6	4788.8	4794.4
15	4801.1	4800.7	4800.3	4794.5	4791.1	4781.5	4788.9	4794.3
16	4801.1	4800.7	4800.2	4794.5	4791.2	4781.5	4788.9	4794.3
17	4801.1	4800.7	4800.3	4794.5	4791.0	4781.6	4788.9	4794.3
18	4801.1	4800.7	4800.3	4794.5	4790.9	4781.6	4788.9	4794.2
19	4801.1	4800.7	4800.3	4794.5	4790.9	4781.6	4788.9	4794.1
20	4801.0	4800.6	4800.2	4794.8	4790.9	4781.6	4788.9	4794.0
21	4801.1	4800.7	4800.0	4794.8	4790.9	4781.6	4788.9	4793.9
22	4801.0	4800.6	4799.7	4794.8	4790.9	4781.6	4788.9	4793.8
23	4801.0	4800.5	4799.2	4794.8	4791.0	4781.6	4788.9	4793.8
24	4801.0	4800.3	4798.8	4794.8	4791.0	4781.6	4788.8	4793.7
25	4801.1	4800.1	4798.3	4794.8	4791.0	4781.6	4788.8	4793.7
26	4801.0	4799.9	4798.2	4794.8	4791.0	4781.6	4788.8	4793.8
27	4800.9	4799.6	4798.0	4794.8	4791.1	4781.6	4788.8	
28	4800.8	4799.3	4797.7	4794.8	4791.1	4781.6	4788.7	
29	4800.7	4799.0	4797.5	4794.8	4791.1	4781.6	4788.6	
30	4800.5	4798.9	4797.4	4794.8	4791.1	4781.6	4788.5	
31	4800.4	4798.8	4797.3	4794.8	4791.1	4781.6	4788.5	
32	4800.2	4798.7	4797.0	4794.8	4791.0	4781.5	4788.4	
33	4799.9	4798.6	4796.9	4794.8	4791.1	4781.5	4788.4	
34	4799.9	4798.6	4796.6	4794.8	4791.1	4781.5	4788.3	
35		4798.5	4796.1	4794.8	4791.1	4781.5	4788.2	
36		4798.4	4795.7	4794.8	4791.1		4788.2	
37		4798.4	4795.5	4794.8	4791.1		4788.3	
38		4798.3	4795.4	4794.8	4791.2		4788.2	
39		4798.3	4795.2	4794.8	4791.2			
40		4798.2	4794.8	4794.8	4791.2			
41		4798.1	4794.6	4794.8	4791.3			
42		4798.0	4794.5	4794.8	4791.2			
43		4798.0	4794.2	4794.8				
44		4797.9	4794.1	4794.8				
45		4797.7	4794.1	4794.8				
46		4797.4	4794.0	4794.8				
47		4797.1	4793.9	4794.5				
48		4796.7	4793.8	4794.5				
49		4796.3	4793.7	4794.5				
50		4796.0	4793.7	4794.5				
51		4795.9	4793.6	4794.5				
52		4795.8	4793.6	4794.5				
53		4795.7	4793.5					

Table A. 2: Sound Velocity Profile Data (ft/sec) for December 5, 2006 - March 29, 2007.

Depth	12/05/2006	12/06/2006	12/12/2006	12/13/2006	12/14/2006	03/28/2007	03/29/2007
1	4723.1	4718.9	4715.0	4718.1		4781.0	
2	4722.9	4718.9	4713.9	4718.1		4777.9	4808.5
3	4722.4	4719.1	4713.3	4718.1	4720.2	4774.9	4808.0
4	4721.8	4719.3	4712.8	4718.1	4720.2	4772.3	4807.5
5	4721.8	4719.3	4712.5	4718.1	4720.2	4771.9	4807.4
6	4721.7	4719.4	4712.2	4718.2	4720.2	4771.3	4807.3
7	4721.6	4719.4	4712.2	4718.3	4720.3	4769.7	4806.9
8	4721.7	4719.5	4712.1	4718.4	4720.2	4766.3	4806.4
9	4721.6	4719.4	4712.1	4718.4	4720.3	4764.6	4805.8
10	4721.4	4719.4	4712.1	4718.5	4720.3	4763.9	4804.7
11	4721.2	4719.4	4712.1	4718.4	4720.4	4763.9	4802.2
12	4720.9	4719.4	4712.1	4718.4	4720.4	4763.9	4800.1
13	4720.9	4719.4	4712.1	4718.4	4720.4	4763.8	4797.6
14	4720.8	4719.4	4712.1	4718.4	4720.4	4763.8	4796.5
15	4720.8	4719.4	4712.1	4718.4	4720.5	4763.8	4795.5
16	4720.7	4719.4	4712.1	4718.4	4720.2	4763.7	4794.7
17	4720.7	4719.4	4712.0	4718.4		4763.4	4793.8
18	4720.6	4719.5	4712.0	4718.4		4762.9	4792.4
19	4720.5	4719.5	4711.9	4718.4		4762.6	4791.2
20	4720.6	4719.6	4712.0	4718.3		4761.5	4789.8
21	4720.6	4719.6	4711.9	4718.1		4761.0	4788.4
22	4720.5	4719.6	4711.9	4718.0		4760.9	4787.5
23	4720.5	4719.7	4711.8	4717.8		4760.8	4787.1
24	4720.5	4719.8	4711.8	4717.7		4760.7	4786.7
25	4720.5	4719.7	4711.8	4717.8		4760.7	4786.1
26	4720.5	4719.8	4711.7	-		4760.7	4785.3
27	4720.4	4719.7	4711.7			4760.7	4784.3
28	4720.3	4719.7	4711.7			4760.6	4782.6
29	4720.3	4719.7	4711.7			4760.6	4781.4
30	4720.3	4719.7	4711.8			4760.5	4780.4
31	4720.4	4719.7	4711.8			4760.5	4779.4
32	4720.4	4719.7	4711.8			4760.5	4779.2
33	4720.3	4719.7	4711.8			4760.5	4779.1
34	4720.3	4719.9	4711.8			4760.4	4779.0
35	4720.4	4719.9	4711.8			4760.4	4778.7
36	4720.4	4719.9	4711.9			4760.4	4778.1
37	4720.4	4720.0	4711.9			4760.4	4777.3
38	4720.4	4720.0	4711.9			4760.4	4776.5
39		4719.8	4711.9			4760.3	4776.1
40			4712.0			4760.3	4775.6
41			4711.9			4760.2	4775.1
42			4712.0				4774.7
43			4711.8				4774.3
44							4774.0
45							4773.8
46							4773.2
47							4773.0
48							4773.0
49							4772.7
50							4772.5
51							4772.4

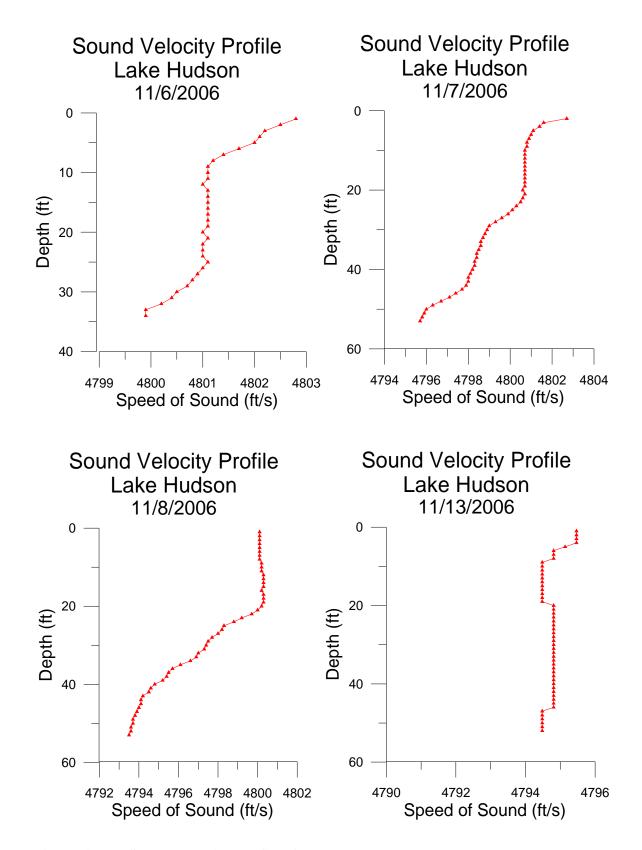


Figure A. 1: Sound Velocity Profiles for November 6, 7, 8, and 13, 2006.

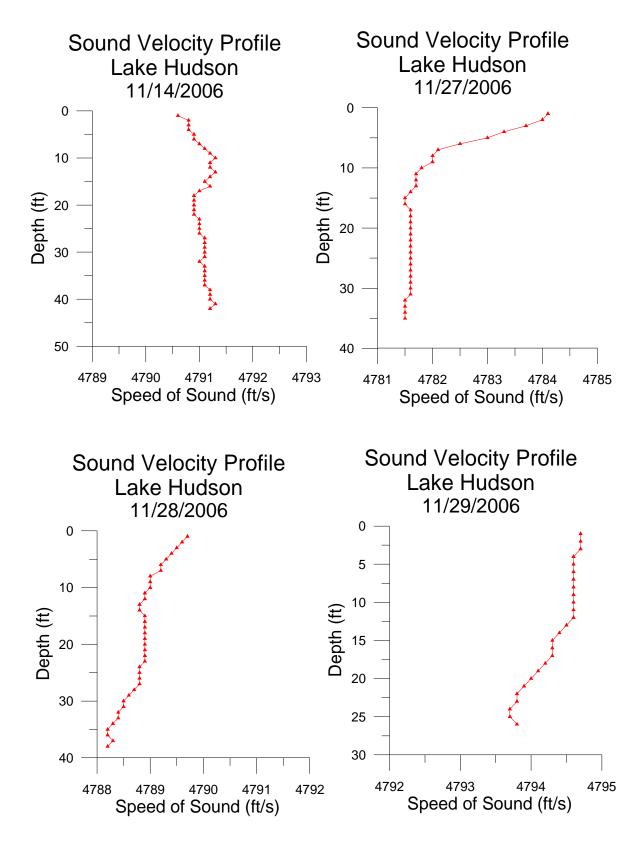


Figure A. 2: Sound Velocity Profiles for November 14, 27, 28, and 29, 2006.

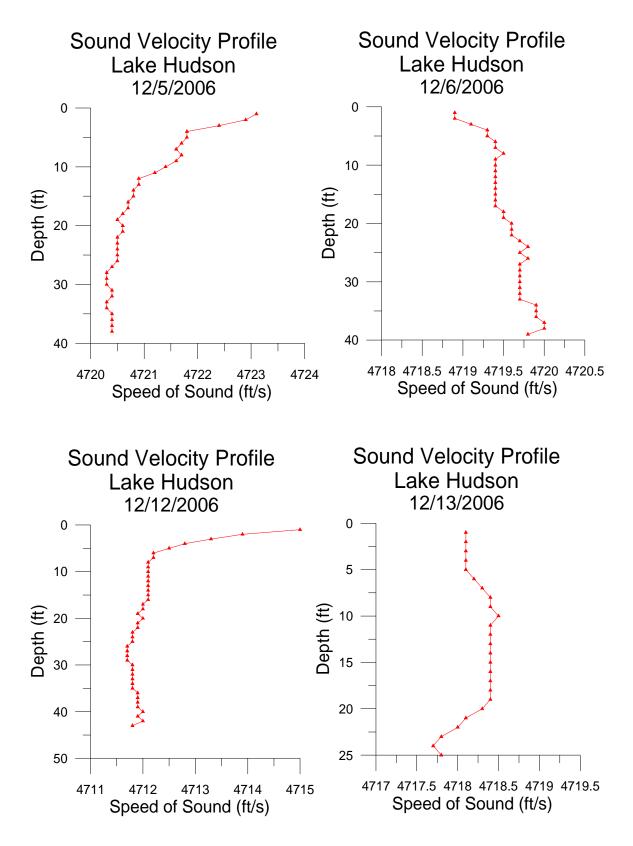
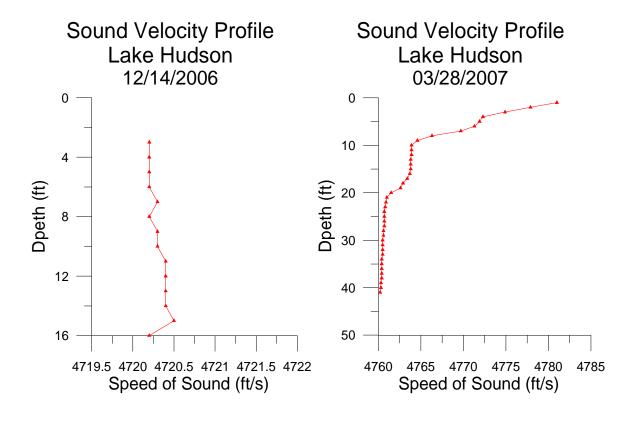


Figure A. 3: Sound Velocity Profiles for December 5, 6, 12, and 13, 2006.



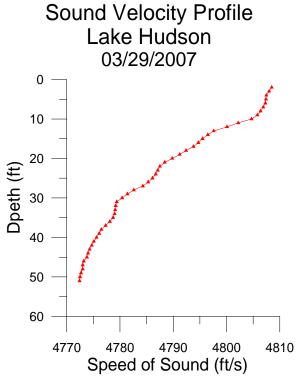


Figure A. 4: Sound Velocity Profiles for December 14, 2006 and March 28 and 29, 2007.

APPENDIX B: Area-Capacity Data

Table B. 1: Lake Hudson Capacity/Area by 0.1-ft Increments.

LAKE HUDSON CAPACITY-AREA TABLE **OKLAHOMA WATER RESOURCES BOARD** 2006-2007 Survey Capacity in acre-feet by tenth foot elevation increments Area in acres by tenth foot elevation increments Elevation .24 .54 .04 .14 .34 44 .64 .74 .84 .94 (ft NGVD) 0.000 0.000 0.000 0.001 0.001 0.002 0.003 0.004 0.006 0.008 554 Area Capacity 0.000 0.001 0.002 0.004 0.007 0.009 0.012 0.014 0.017 0.020 555 Area 0.010 0.012 0.015 0.018 0.021 0.025 0.029 0.033 0.037 0.042 0.023 0.026 0.029 0.032 0.035 0.038 0.041 0.044 0.048 0.052 Capacity 556 0.048 0.054 0.060 0.067 0.074 0.082 0.090 0.099 0.108 Area 0.119 Capacity 0.056 0.060 0.065 0.070 0.075 0.081 0.087 0.093 0.099 0.105 557 Area 0.130 0.141 0.153 0.166 0.181 0.196 0.213 0.233 0.257 0.284 0.119 0.163 0.186 0.253 0.291 0.112 0.127 0.135 0.146 0.216 Capacity 558 0.32 0.35 0.39 0.43 0.48 0.53 0.59 0.65 0.71 0.78 Area Capacity 0.33 0.37 0.41 0.45 0.49 0.54 0.58 0.62 0.67 0.71 559 0.95 1.04 1.14 1.24 1.44 1.55 1.66 1.77 Area 0.86 1.34 0.88 0.91 0.94 0.97 1.00 1.03 1.05 1.08 1.12 1.15 Capacity 560 1.89 2.01 2.13 2.39 2.52 2.66 2.80 2.96 3.13 Area 2.26 Capacity 1.18 1.22 1.25 1.29 1.32 1.36 1.40 1.48 1.62 1.85 561 3.33 3.57 3.87 4.22 4.63 5.10 5.64 6.26 6.95 7.73 Area 2.66 3.79 4.42 5.08 5.79 7.32 8.15 2.20 3.21 6.53 Capacity 562 8.6 9.5 10.6 11.7 13.0 14.4 15.9 17.6 19.4 21.5 Area 9.9 12.1 14.6 17.6 19.3 Capacity 9.0 11.0 13.3 16.0 21.2 49.5 563 23.7 26.1 28.7 31.6 34.7 38.0 41.6 45.4 53.8 Area 42.3 Capacity 23.2 25.3 27.4 29.7 32.0 34.4 36.9 39.5 45.4 564 73.0 94.1 101 59.3 66.1 0.08 87.0 108 116 123 Area Capacity 67.4 68.3 69.3 70.1 70.6 71.2 71.7 72.3 72.8 73.4 565 130 138 145 153 160 168 176 184 191 199 Area Capacity 73.9 74.5 75.1 75.6 76.2 76.8 77.3 78.0 78.7 79.6 566 207 215 224 232 240 249 258 267 276 285 Area Capacity 80.7 81.8 83.0 84.2 85.4 86.6 87.9 89.2 90.5 91.8 567 Area 294 303 313 323 333 343 354 365 376 387 93.4 95.2 97.1 99.3 102 104 107 114 117 Capacity 110 568 399 412 437 451 465 479 494 509 525 Area 424 Capacity 121 125 128 132 137 141 145 150 154 159 569 542 562 583 604 625 646 667 688 710 732 Area 201 204 206 208 210 212 214 216 218 219 Capacity 776 799 844 570 754 821 867 890 914 937 961 Area Capacity 221 223 225 227 229 231 233 235 237 239 571 985 1009 1034 1058 1083 1108 1133 1159 1185 1211 Area 243 245 247 250 252 254 256 258 Capacity 241 261 572 1237 1263 1290 1317 1344 1372 1399 1427 1456 1484 Area Capacity 263 265 268 270 273 276 278 281 284 287 573 1542 1724 1755 1787 Area 1513 1572 1601 1631 1662 1693 290 293 299 303 306 313 316 320 Capacity 296 309 574 1820 1855 1890 1926 1961 1997 2033 2069 2105 2142 Area 350 356 348 352 354 358 360 362 364 Capacity 366

Table B. 2: Lake Hudson Capacity/Area by 0.1-ft Increments (cont).

LAKE HUDSON CAPACITY-AREA TABLE **OKLAHOMA WATER RESOURCES BOARD** 2006-2007 Survey Capacity in acre-feet by tenth foot elevation increments Area in acres by tenth foot elevation increments Elevation (ft NGVD) .04 .14 .24 .34 .54 .64 .74 .84 .94 Area Capacity Area <u>4</u>16 Capacity Area Capacity Capacity Area Capacity Area Capacity

Table B. 3: Lake Hudson Capacity/Area by 0.1-ft Increments (cont).

LAKE HUDSON CAPACITY-AREA TABLE **OKLAHOMA WATER RESOURCES BOARD** 2006-2007 Survey Capacity in acre-feet by tenth foot elevation increments Area in acres by tenth foot elevation increments Elevation (ft NGVD) .04 .14 .24 .34 .44 .54 .64 .74 .84 .94 Area Capacity Area

Table B. 4: Lake Hudson Capacity/Area by 0.1-ft Increments (cont).

Capacity

LAKE HUDSON CAPACITY-AREA TABLE OKLAHOMA WATER RESOURCES BOARD

2006-2007 Survey

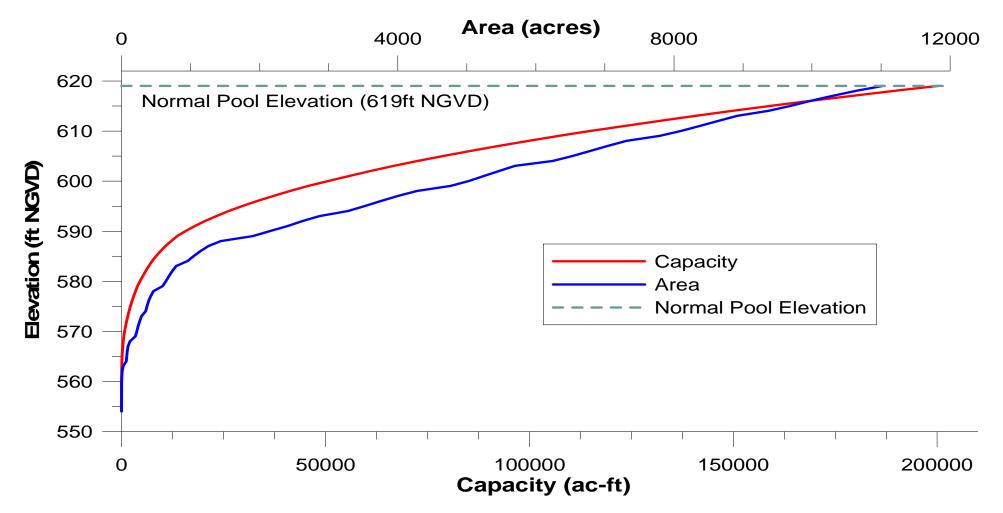
Capacity in acre-feet by tenth foot elevation increments

Area in acres by tenth foot elevation increments

Elevation											
(ft NGVD)		.04	.14	.24	.34	.44	.54	.64	.74	.84	.94
617	Area	179361	180394	181428	182466	183505	184548	185594	186642	187693	188747
	Capacity	10304	10331	10358	10385	10412	10439	10467	10495	10523	10551
618	Area	189806	190872	191942	193015	194092	195172	196256	197342	198433	199527
	Capacity	10645	10679	10714	10748	10782	10817	10851	10886	10921	10956
619	Area	200185									
	Capacity	11029									

Figure B. 1. Capacity-Area Curve

Lake Hudson Capacity-Area by Elevation 2007 Survey



APPENDIX C: Lake Hudson Bathymetric Maps

Figure C. 1: Lake Hudson Bathymetric Map with 5-foot Contour Intervals.

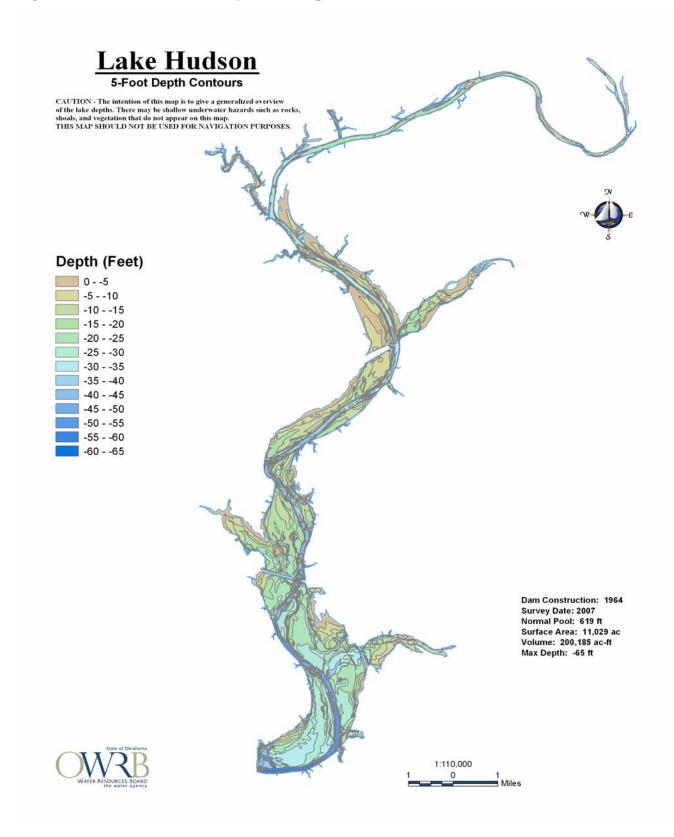


Figure C. 2: Lake Hudson Shaded Relief Bathymetric Map.

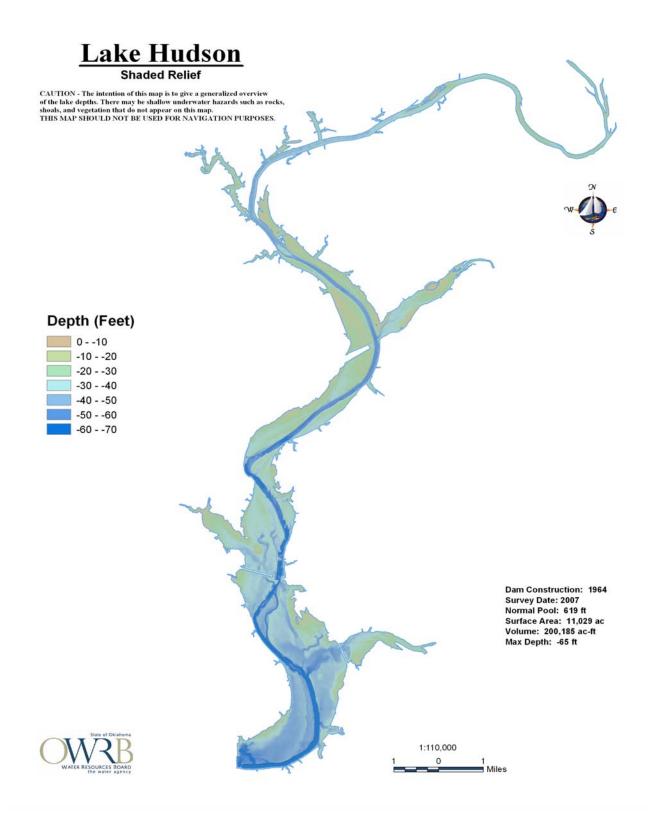


Figure C. 3: Lake Hudson Collected Data Points.

